

ENERGY HARVESTING TRANSDUCERS -ELECTROMAGNETIC (ICT-ENERGY SUMMER SCHOOL 2015)

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Energy Harvesting System Overview



- An energy harvesting system consists of an energy capture mechanism (e.g. a cantilever beam, wind turbine), an electromechanical transducer (e.g. piezoelectric material), power conditioning circuitry, and usually temporary energy storage all of which delivers electrical power to a some electronic load.
- Each subsystem influences the behavior of the subsystem both immediately upstream and downstream in the overall system. The energy capture mechanism even affects the environment in which it operates, although this effect may be small.
- This lecture will discuss the transduction block



Three Types of Electromechanical Lossless Transduction

- 1. <u>Electrodynamic</u> (also called <u>electromagnetic</u> or inductive): motor/generator action is produced by the current in, or the motion of an electric conductor located in a fixed transverse magnetic field (e.g. voice coil speaker)
- 2. <u>Piezoeletric</u>: motor/generator action is produced by the direct and converse piezoelectric effect dielectric polarization gives rise to elastic strain and vice versa (e.g. tweeter speaker)
- **3.** <u>Electrostatic</u>: motor/generator action is produced by variations of the mechanical stress by maintaining a potential difference between two or more electrodes, one of which moves (e.g. condenser microphone)

Credit: This classification and much of the flow from Electromagnetic section is based on the 2013 PowerMEMS presentation by Prof. David Arnold at the University of Florida



Outline for Short Course

- Introduction and Linear Energy Harvesting
- Energy Harvesting Transducers
 - Electromagnetic
 - Piezoelectric
 - Electrostatic
- Wideband and Nonlinear Energy Harvesting
- Applications



FUNDAMENTALS OF ELECTROMAGNETIC TRANSDUCTION



Electromagnetic Transduction

1. <u>Electromagnetic Transduction</u>: motor action produced by the current in an electric conductor located in a fixed transverse magnetic field



$$F = Bli$$



Voice coil speaker



Permanent magnet motor



Electromagnetic Vibration Energy Harvesting

- Generally uses permanent magnet and coil
- Voltage induced by time rate of change of flux Faraday's Law

$$V = -N \frac{d\Phi}{dt}$$

where N is the number of coil turns and Φ is the magnetic flux



Williams et. al, IEEE Proc. Circuits Devices Syst., 2001



Beeby et. al, JMM, 2007



Common Electromagnetic VEH Architecture



Figure 6. Magnet dimensions for simulation results.

Beeby et. al, JMM, 2007



Electromagnetic VEH Theory

Faraday's Law

$$V = -\frac{d\Phi}{dt}$$

 $\Phi~$ is the total flux through a surface

We can get to the get to the voltage in one of two ways

$$V_{tr} = -\int_{S} \frac{\partial \boldsymbol{B}}{\partial t} \cdot d\vec{\boldsymbol{s}}$$

which is from the perspective of the coil and assumes the flux is changing

$$V_m = \oint_C (\vec{v} \times \boldsymbol{B}) \cdot d\vec{l}$$

which is from the perspective of the B-field and assume the coil is moving

Either of these methods should give the same answer



A Simple Example

A square coil moves relative to an orthogonal B-field (or the magnet moves relative to the coil, it doesn't matter):



l is the length of the side of the coil *z* is the distance of the length of the coil in the B-field

$$V_m = V = \oint_C (\vec{v} \times B) \cdot d\vec{l} = \dot{z}Bl$$

Or for N coils:

$$V(t) = NBl\dot{z}(t)$$

NBl is often referred to as the "transformation factor"



Power Output from a EM Harvester

Electric circuit



V is the voltage generated by the coil L is coil inductance Rc is coil resistance Zl is load impedance

But usually, frequencies are low so inductance can be ignored, and power output is calculated through a resistor



$$P_{rms} = \frac{1}{2} \frac{|V_0|^2}{R_l}$$
$$|V_0| = |V| \frac{R_l}{R_c + R_l}$$
$$P_{rms} = \frac{1}{2} \frac{|V|^2 R_l}{(R_c + R_l)^2}$$



Power Output from a EM Harvester



From the previous simple example

$$V(t) = NBl\dot{z}(t)$$

So:

$$P_{rms} = \frac{1}{2} \frac{(NBl)^2 R_l}{(R_c + R_l)^2} |\dot{z}|^2 = \frac{1}{2} \frac{(NBl)^2 R_l}{(R_c + R_l)^2} \omega^2 Z_0^2$$

where Z_0 is the relative displacement magnitude

For reasons that will become apparent, we will write this as:

$$P_{rms} = \frac{1}{2} \frac{(NBl)^2}{R_c + R_l} \frac{R_l}{R_c + R_l} \omega^2 Z_0^2$$



EM Harvester Mechanics

Lorentz Force:

$$F = \boldsymbol{I} \oint_C d\boldsymbol{l} \times \boldsymbol{B}$$

For our simple example, this reduces to

$$F(t) = NBli(t)$$
$$i(t) = \frac{V(t)}{R_c + R_l} = \frac{NBl}{R_c + R_l} \dot{z}(t)$$
$$F(t) = \frac{(NBl)^2}{R_c + R_l} \dot{z}(t)$$



EM Harvester Mechanics

Remember from Linear VEH theory

$$m\ddot{z} + (b_m + b_e)\dot{z} + kz = -m\ddot{y}$$

where $b_e \dot{z}$ is the electrically induced force. Substituting:

$$m\ddot{z} + b_m\dot{z} + \frac{(NBl)^2}{R_c + R_l}\dot{z} + kz = -m\ddot{y}$$

And we can say:

$$b_e = \frac{(NBl)^2}{R_c + R_l}$$



Governing Equations and System Models

The governing equations for the Electromagnetic VEH are:

$$m\ddot{z} + b_m\dot{z} + \frac{(NBl)^2}{R_c + R_l}\dot{z}(t) + kz = -m\ddot{y}$$

$$V_0(t) = NBl \frac{R_l}{R_c + R_l} \dot{z}(t)$$

where the independent states of the system are: z and \dot{z} or V_o

and the power is given by:

$$P_{rms} = \frac{1}{2} \frac{(NBl)^2}{R_c + R_l} \frac{R_l}{R_c + R_l} \omega^2 Z_0^2 = \frac{1}{2} b_e \frac{R_l}{R_c + R_l} \omega^2 Z_0^2$$



Interesting Points

- The electromechanical force is actually in phase with velocity (disregarding coil inductance) and so the VDRG model matches electromagnetic harvesters well
- If coil resistance were zero, power output would exactly match the maximum possible power predicted by the VDRG model
- For a fixed coil resistance, power output is maximized for $R_l = R_c$
 - But this is not max "efficiency". So, max power and max efficiency are not the same operating point.
- The simplified algebraic relationships don't hold exactly for more complex geometry, but the basic principles do



DEVICE EXAMPLES



Self-powered Watches

Seiko











3D drawing of the MGS Watch



A Way to Get Rid of the Gears



Figure 2: Schematic of the energy-harvesting generator with a single rotor disk.



Figure 6: Prototype photo. The added eccentric weight is partially covering the permanent magnets. A US quarter coin was added for size comparison purposes.

Romero et. al., IEEE MEMS, 2011





Figure 1. Under certain conditions linear vibration causes movement of the pendulum.



Figure 7. Prototype of an inductive non-resonant vibration transducer.

Spreemann et. al., JM&M, 2006



Earliest Linear EM VEHs





Shearwood and Yates, Electronics Letters., 1997

Mitcheson et. al., JMEMS, 2004



Southampton and Perpetuum



Perpetuum



Beeby et. al, JMM, 2007



Multi-pole Magnet Generators



Figure 4. Picture and schematic of the prototype four-pole energy harvester.

Cheng and Arnold, JMM, 2010



Multi-pole Magnet Generators



Roundy and Takahashi, Sensors & Actuators, 2013



EnOcean Light Switch



EnOcean, www.enocean.com



Impact Based



Miah and Park, Energy Conversion & Management, 2015



Wearable



Figure 1. Photograph (left) and 3-D schematic (right) of the energy harvester.

Rao et. al., PowerMEMS, 2013



Summary

- First commercially successful energy harvesters have been electromagnetic
 - Watches
 - Perpetuum
- High coupling is achievable at sizes cm³ and above
- Voltages (and source impedance) tend to be low
- Few micro-scale implementations

